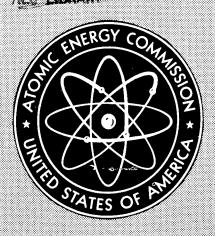
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ALLOYING CHARACTERISTICS OF THE RARE EARTH ELEMENTS WITH THE TRANSITION ELEMENTS

Final Report, March 15, 1962 — April 30, 1964

By Rodney P. Elliott

April 30, 1964

Illinois Institute of Technology IIT Research Institute Chicago, Illinois

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ALLOYING CHARACTERISTICS OF THE RARE EARTH ELEMENTS WITH THE TRANSITION ELEMENTS

March 15, 1962 to April 30, 1964

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United States Atomic Energy Commission Metallurgy and Materials Programs Division of Research Washington 25, D. C.

ALLOYING CHARACTERISTICS OF THE RARE EARTH ELEMENTS WITH THE TRANSITION ELEMENTS

ABSTRACT

The alloying characteristics of the rare earth elements with the transition metals undergo a radical change as the atomic number of the transition series increases -- transition elements in Groups IVa, Va, and VIa are immiscible with the rare earths, while elements of Groups VIIa, and VIIIa, VIIIb, and VIIIc form many compounds. Since this cannot be correlated with a size effect, a reasonable explanation for this behavior is a valency or electronegativity effect. Those binary systems forming compounds form "Laves phases," which can exist in one of three related crystal structure types: MgCu2, MgZn2, or MgNi2. The specific Lavestype crystal structure can be related to the average free electron concentration, a phenomenon which has been used to calculate electronic valency of the transition elements. A compilation of the known Laves-type phases occurring between rare earth elements and transition metals supports the hypothesis that the valency effect is operative. Forty-two additional rare earth-transition metal compounds previously unknown have been prepared and found to be consistent with the previously noted trend with but two exceptions.

On the assumption that a critical electron/atom ratio determines which Laves-type structures are stable, the periodical grouping of the Laves-type species of the rare earth-transition metal compounds indicates a slight but regular increase in valency as the atomic number of the rare earth increases. Ternary alloys prepared between the Laves phases of different structure types substantiate the observed valency trend.

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ALLOYING CHARACTERISTICS OF THE RARE EARTH ELEMENTS WITH THE TRANSITION ELEMENTS

I. INTRODUCTION

Although the rare earth elements are chemically very similar, they present a dichotomy with respect to alloying behavior with the transition elements. Known binary systems with Groups IVa, Va, and VIa elements form no compounds—the systems often display immiscibility in the liquid as well as the solid state. Alloys with the Group VIIa, VIIIa, VIIIb, and VIIIc elements form numerous intermetallic compounds. This complete change in alloying behavior apparently is not related to the size factor phenomenon, but to valency or electronegativity effects.

Because of the basic similarity of the properties of the rare earths, a unique group of elements is available for alloy theory studies. Since the rare earth elements are transition elements, the results of such studies are immediately applicable to that group of metals from which most of the modern alloys are fabricated.

The analysis of alloy formation was first discussed by Hume-Rothery, who found that certain compounds of known crystal symmetry could be rationalized in terms of their electron/atom ratio using the common valences associated with chemical compounds. These compounds have subsequently been termed "Hume-Rothery compounds." Attempts to analyze solid solution formation and intermetallic compound formation of less noble metal systems using the concepts of Hume-Rothery have been less successful. This is understandable since the Hume-Rothery compounds are metallic and stability is governed by free electron effects rather than by ionic characteristics.

Specific types of intermetallic compounds are known to occur in binary systems having similar metallurgical properties. In most instances such occurrences do not permit detailed calculations to be made with regard to their specific alloying characteristics. A notable exception to this, however, is the Laves phases--i.e., intermetallic

compounds having crystal structures isotypic with $MgCu_2$, $MgZn_2$, and $MgNi_2$.

There is a marked similarity among the crystal lattices of the three Laves-type compounds. For the AB₂ prototype compounds, with respect to the A atom, MgCu₂ consists of double layers of hexagonal arrays of A atoms stacked abcabc; MgZn₂ consists of double layers of A atoms stacked ababab; and MgNi₂ consists of double layers of A atoms stacked abacabac. The B atoms surround the A atoms in tetrahedra. The manner in which these tetrahedra are connected is dependent on the particular crystal type.

The existence of Laves phases is governed primarily by space-filling considerations. For these structures the theoretical atomic diameter ratio is 1.225; however, Laves phases are known for the d_A/d_B spectrum from 1.05 to 1.68, although the great majority occur between 1.12 to 1.38. * It has been adequately demonstrated by Dwight⁽¹⁾ that there is no correlation between the Laves phase structure type and the atomic diameter ratio.

Electronic factors have been shown to be operative governing which crystal type of the Laves phases is stable. In a series of projects over a 3 1/2 year period at IIT Research Institute (2-4) it has been demonstrated that for a common A element the structure type goes through the sequence $MgCu_2 \longrightarrow MgZn_2 \longrightarrow MgCu_2$ as the B element increases in atomic number for a given period. Examples of this behavior are shown for zirconium, columbium, and hafnium with elements of the first transition series in Figure 1. The full sequence is not observed for the A elements titanium and tantalum, because the size factor becomes conducive to continuous or extended solid solutions. The nonoccurrence of Laves phases for binary systems of transition elements with nickel is not satisfactorily explained, but it probably due to electronic considerations.

^{*}For discussion of the theoretical atomic diameter ratio and the description of the crystal structures, the reader is referred to W. Hume-Rothery and G. Raynor, "The Structure of Metals and Alloys," Institute of Metals, London, 1954, 227-237.

Binary Laves phases alloy readily with each other. Ternary alloys between binary compounds of different crystal structure show but a narrow composition region that is two-phase. Ternary alloys between MgCu, structures at the extremes of the sequence show an intermediate compositional region in which alloys have the MgZn2 structure. The latter phenomenon is further substantiation of the dependence of the crystal structure of Laves phases on the electronic rather than on the atomic diameter ratio. From such it may also be concluded that the electron valency of elements for a given transition series varies monotonically with the atomic number. Witte (5) has calculated electron/atom volumes of Brillouin zones for Laves phase compounds and shows tangencies of the Fermi sphere for the MgCu₂ structure at an electron/atom ratio of 1.83, and 1.93 and 2.32 for the Mg Zn₂ structure. The value 1.83 is consistent with the 1.80 observed experimentally by Laves and Witte (6) by diluting the prototype phases with aluminum, zinc, silver, and silicon, and using the common metallic valencies in the calculations. Elliott and Rostoker (4) have applied the electron/atom ratios of 1.80 and 2.32 to calculate a consistent set of valencies for the transition elements assuming 4 for titanium. Further work by Elliott (3) showed that it is impossible to use such methods for calculating a complete set of consistent valencies since other variables affect the composition limits.

Laves-type phases occur regularly in alloys of the rare earth metals with the transition metals. Dwight⁽¹⁾ has inferred that the sequence $\mathrm{MgCu_2} \longrightarrow \mathrm{MgZn_2} \longrightarrow \mathrm{MgCu_2}$ is likewise operative for rare-earth base Laves-type phases. As yet, however, the complete sequence has not been observed experimentally. The present investigation was undertaken with two objectives in mind: (a) to prepare binary Laves phases between the rare earth elements and the transition metals so that the $\mathrm{MgCu_2} \longrightarrow \mathrm{MgZn_2} \longrightarrow \mathrm{MgCu_2}$ sequence could be more precisely positioned as to its dependence on the periodic table (and hence, valency), and (b) to prepare ternary Laves phases between these binary compounds to ascertain the relative valencies of the rare earth elements on the assumption that the $\mathrm{MgCu_2} \longrightarrow \mathrm{MgZn_2} \longrightarrow \mathrm{MgCu_2}$ transitions occur at known electron/atom ratios.

II. EXPERIMENTAL TECHNIQUES

Materials of the highest available purity were obtained for the production of alloys. The purity, form, and supplier of these materials are listed in Table I.

Wherever feasible, nonconsumable arc-melting techniques were used in preparing the alloy compositions. The form of the as-received material dictated, in part, the melting technique. Many of the rare earths were available as sponge, which is powdery. Sponge and transition metal powders were blended and compacted prior to arc melting. Powder was prepared by filing those transition metals not available as powder. If the rare earth was available as solid material, the arc-melting technique used was to place the higher melting constituent on top of the lower melting constituent before melting. Because of the expensive nature of the component materials, small ingots weighing 3 grams were produced. Ingots were remelted several times to insure homogeneity of composition. After melting, the ingots were annealed 16 hr at 1000°C in argon to eliminate any microinhomogeneities resulting from peritectic formation of intermetallic compounds.

The wide divergence of the melting points of the component elements made arc-melting techniques unsuitable in many instances. Electron beam melting, levitation melting, and very high pressure sintering were attempted unsuccessfully; the latter because of temperature limitations of equipment. Liquid-phase sintering in columbium crucibles was effective for alloys containing osmium, ruthenium, or rhenium. In these instances the rare earth metal was pickled, the alloy charge weighed, and the columbium crucible welded closed in a helium atmosphere. In other instances liquid phase sintering in boron nitride crucibles, or graphite crucibles with boron nitride liners, was effective. Alloys prepared by liquid-phase sintering were, in general, not as homogeneous as those prepared by arc melting.

Annealed specimens were prepared for diffraction studies by crushing in a steel mortar. Powder of -200 mesh was used. Powder patterns were indexed by Hull-Davey charts. Accurate lattice parameters

were obtained by an IBM 7090 least-squares program in which the systematic absorption error proportional to the trigonometric Nelson-Riley function was incorporated.

III. EXPERIMENTAL RESULTS

The results of X-ray investigations of binary AB₂ compositions are summarized in Tables II and III. These data, together with the previously known data for Laves-type compounds, are shown graphically with respect to the periodic table in Figures 3, 4, and 5.

The results of the X-ray investigation of ternary alloys of AB₂ composition are summarized in Table IV and shown graphically in Figures 6, 7, and 8. The dots in these Figures indicate those compositions actually prepared.

IV. DISCUSSION

A. Binary Laves Phases

As is evident in Figures 3, 4, and 5, the structure type of known Laves phases is distributed regularly as a function of the periodic table. The only exceptions to this are NdMn₂ and SmMn₂ which were both found and verified to have the MgZn₂ structure in a field where the MgCu₂ structure is more probable. From a scrutiny of distribution of the MgCu₂ and MgZn₂ structures, several important conclusions are made:

- l. Laves-type phases exist with regularity with all rare earth elements for the transition elements in Groups VIIa, VIIIa, VIIIb, and VIIIc. Since the d_A/d_B ratio is favorable for all combinations, the nonexistence of Laves-type phases must be attributed to either (a) electronic considerations-that is, an unfavorable electron/atom ratio--or (b) free energy or electronegativity restrictions imposed by the system.
- 2. While the great majority of rare earth Laves phases are of the MgCu₂ type, the existence of the MgZn₂ type of

structure occurs in such a pattern as to indicate that the transition ${\rm MgCu}_2 \longrightarrow {\rm MgZn}_2 \longrightarrow {\rm MgCu}_2$ exists. Thus the electronic valency governs which type of structure is stable. The complete ${\rm MgCu}_2 \longrightarrow {\rm MgZn}_2 \longrightarrow {\rm MgCu}_2$ transition, however, is in no instance observed.

- 3. For a given transition element period there is the tendency for the MgZn₂ ->MgCu₂ discontinuity to move to the right (that is, to higher atomic number) as the rare earth A element increases in atomic number. On the assumption that the electron valency decreases as the atomic number of the transition element period increases, the discontinuity shift suggests that there is a slight but regular increase in valency as the atomic number of the rare earth increases.
- 4. In comparison of the three transition series, the discontinuity between the ${\rm MgZn_2}$ and the ${\rm MgCu_2}$ types shifts from left to right in going from the first to the second transition series, and from rare earths of high atomic number to low atomic number in going from the second transition series to the third transition series. Such shifts suggest a net increase in valency for a given periodic group in successive periods (e.g., ${\rm v_{Fe}} < {\rm v_{Ru}} < {\rm v_{Os}}$).

B. Ternary Alloys

The periodic variation of structure type was indicative of the controlling factor of the free electron concentration. Ternary alloys were necessary to amplify the binary findings so that quantitative calculations could be made. Ternary alloys were made on the basis of the binaries to provide information regarding (a) the relative valencies for the rare earths, (b) the reasons for the nonoccurrence of the complete MgCu₂ —> MgCu₂ trend, and (c) the reasons for the nonexistence of Laves phases, or indeed, compounds for the rare earths with transition metals of groups IVa, Va, or VIa.

The valencies of the rare earth metals may be calculated from the miscibility between the binary Laves phases in Figure 6a-6f,

and Figure 7d-7e. The basis of the calculations are (a) that the ${\rm MgCu_2}$ -structure miscibility limit is electron dependent and exists at the electron/ atom ratio of 1.80 as given by Witte⁽⁵⁾, and (b) that the free electron valencies of the transition metals calculated by Elliott and Rostoker⁽³⁾ on this assumption are applicable--namely, ${\rm v_{Ti}}=3.92, {\rm v_{V}}=2.19, {\rm v_{Cr}}=1.69, {\rm v_{Mn}}=1.35, {\rm v_{Fe}}=0.92, {\rm v_{Co}}=0.72, {\rm and v_{Ni}}=0.25.$ The existence of the ${\rm MgZn_2}$ -type structure for ${\rm NdMn_2}$ and ${\rm SmMn_2}$ could not be incorporated in such a treatment.

From Figure 7d and 7e, the limits of the MgCu₂ miscibility are taken as 25 a/o ErMn₂ for the Er(Mn + Fe)₂ ternary, and 45 a/o TmMn₂ for the Tm(Mn + Fe)₂ ternary. Therefore,

$$V_{Er}$$
 + 2(0.75 v_{Mn} + 0.25 v_{Fe}) = 3 x 1.80
 V_{Er} + 2(0.75 x 1.35 + 0.25 x 0.92) = 3 x 1.80
 v_{Er} = 2.92 electrons/atom

and,

$$V_{Tm}$$
 + 2(0.55 v_{Mn} + 0.45 v_{Fe}) = 3 x 1.80
 V_{Tm} + 2(0.55 x 1.35 + 0.45 x 0.92) = 3 x 1.80
 v_{Tm} = 3.08 electrons/atom

It is therefore quite apparent that the accuracy with which the valencies may be calculated is very dependent upon the accuracy with which the limit of the ${\rm MgCu}_2$ miscibility range may be defined. The accuracy of ${\rm v}_{\rm Er}$ is thus more precisely defined than ${\rm v}_{\rm Tm}$ by the above calculations.

From the calculated value of v_{Er} , the values of v_{Sm} , v_{Gd} , v_{Dy} , and v_{Ho} may be calculated from the miscibility ranges shown in Figures 6a-6d. For example,

0.55
$$v_{Dy}$$
 + 0.45 v_{Er} + 2 v_{Mn} = 3 x 1.80
0.55 v_{Dy} + 0.45 x 2.92 + 2 x 1.35 = 3 x 1.80
 v_{Dy} = 2.53 electron/atom

Similarly, $v_{Sm} = 2.04$, $v_{Gd} = 2.04$, and $v_{Ho} = 2.68$ electrons/atom.

The limit of the ${\rm MgCu}_2$ miscibility may be calculated for the ternary system (Dy + Tm)Mn₂ in Figure 6e using these valencies. Assuming M to be the mol fraction of ${\rm TmMn}_2$

$$M \times v_{Tm}$$
 + (1-M) v_{Dy} + 2 x v_{Mn} = 3 x 1.80
 $M \times 3.00$ + (1-M) 2.53 + 2 x 1.35 = 3 x 1.80
 $M = 0.36$, 36 a/o TmMn₂

which is in good agreement with the experimentally observed limit of miscibility.

The free electron valencies calculated increase regularly as the atomic number of the rare earth element increases (Figure 9).

The calculated limit of the MgCu₂ structure for the (Ho + Tm)Mn₂ system is 6 a/o TmMn₂. The experimentally observed limit (Figure 6e) is >10 a/o TmMn₂. The inconsistency of this system with the others is readily discernible by comparing it with the (Ho + Er)Mn₂ system. Since thulium has a higher valency than does erbium, less dilution of HoMn₂ with thulium than erbium should be required to bring the electron/ atom ratio to a value greater than 1.80.

From Figure 9, approximate valencies of 1.3 for lanthanum, 1.6 for neodymium, and 1.4 for cerium may be taken. Thus, from the ternary (La + Nd)Os₂ (Figure 8a), a valency of ~2.08 for Os is calculable. The limit of the MgCu₂ structure miscibility in the (La + Gd)Os₂ and (Ce + Gd)Os₂ ternaries calculated using these valencies are in only approximate agreement with the experimental data, Figure 8b and 8c. The electron/atom ratio for both LaOs₂ and CeOs₂ is near the critical value 1.80 as could be inferred from the experimental data in Figure 8b and 8c, which show no extended miscibility of the MgCu₂-type structure.

If from Figure 8d the limit of the stability of MgCu $_2$ structure type is taken as 15 a/o CdRu $_2$, a free electron valency of 1.66 is calculated for ruthenium. Thus for the elements of Group VIIIa, $v_{Fe} < v_{Os}$ (0.92 < 1.66 < 2.08), as had been predicted on the basis of the binary alloys.

Calculated valencies of the rare earth elements discussed to this point are consistent within themselves and with the previously calculated valencies of the transition elements. There are several areas where the valencies as calculated, or the electronic theory, present ambiguities.

- On the basis of the previously accepted valency of chromium, and using the calculated valencies of the rare earth elements, the electron/atom ratio of all the binary systems of rare earths with chromium are favorable for the existence of Laves phases. It had been previously established that the size factor was satisfactory.
- 2. The nonexistence of Laves phases of the transition elements with nickel had been interpreted by Elliott and Rostoker (3) to result from an electron/atom ratio below a minimum value, taken as ~1.3. Electron/atom ratios of all the rare earths with nickel are less than 1.3, yet all form Laves phases with nickel.
- 3. Dilution of the MgZn₂-type Laves phases with chromium should cause the electron/atom ratio to increase. At the value 2.32 the structure should revert to the MgCu₂ structure. Such does not occur. ErMn₂, TmMn₂, and LuMn₂ when diluted with chromium (Figure 7a-7c) generate the three-phase field of the MgZn₂ structure, rare earth, and chromium. The electron/atom ratio of the limit of the MgZn₂ structure type is ~2, much less than the assumed value of 2.32 for the condition of Fermi sphere tangency.
- 4. The existence of compounds NdMn₂ and SmMn₂ with the hexagonal, MgZn₂-type structure presents a very confusing picture of the sequence MgCu₂ -> MgZn₂ -> MgCu₂ as observed in all transition metal Laves phases. For compound sequences SmMn₂, SmFe₂, SmCo₂, SmNi₂, and ErMn₂, ErFe₂, ErCo₂, ErNi₂, the MgZn₂ -> MgCu₂ transition is observed. Therefore, presumably both SmMn₂ and ErMn₂

electrons/atom. Alloys between SmMn₂ and ErMn₂ should, therefore, be of the MgZn₂ structure; such is not observed, (Figure 6a). The immiscibility of hexagonal SmMn₂ and ErMn₂ with the intermediate formation of the cubic MgCu₂ structure suggests the unlikely existence of two discrete electron/atom ranges for the MgZn₂ structure. Another possibility is that SmMn₂ and ErMn₂ have the MgNi₂ structure distinguishable from the MgZn₂ structure only by usually weak diffraction lines, the positive identification of which would be difficult unless it is unequivocally established that the prepared compound is single-phase.

$v. \int \underline{SUMMARY}$

On the basis of binary and ternary alloys of the ${\rm MgCu}_2$ and ${\rm MgZn}_2$ structure formed between the rare earth elements and the transition metals, a study of the free electron valency of the rare earth metals has been made. It is found that there is an increase in the valency as the atomic number of the rare earth metal increases.

Experimental data are consistent for ternary systems in which the component binaries have Laves-type phases. The valencies calculated, however, do not permit explanation of the general theory of alloying of rare earth transition metal systems. Stability of Laves-type phases for rare earth chromium systems is predicted but not observed. Similarly, theory indicates the nonexistence of Laves phases between the rare earth metals and nickel; Laves-type phases exist in all instances.

Respectfully submitted,

IIT RESEARCH INSTITUTE

Rodney P. Elliott

Senior Metallurgist

jcr

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TABLE I

RARE EARTH AND TRANSITION METALS PURCHASED

Element	Purity, %	Form	Supplier
Iridium Platinum Palladium Rhodium	99.9+ 99.9+ 99.9+ 99.9+	Sponge Sponge Sponge Sponge	Englehard Industries, Baker Platinum Div.
Ytterbium Terbium Thulium Cerium Lutetium	99.8+ Di	stilled (Ingot) stilled (Ingot) stilled (Ingot) Ingot Sponge	Kleber Laboratories, Inc. (Metals Div.)
Dysprosium Holmium Gadolinium Erbium Lanthanum Praseodymium Neodymium Samarium	99.9+ 99.9+ 99.9+ 99.9+ 99.9+ 99.9+ 99.9+	Sponge Sponge Sponge Sponge Ingot Ingot Ingot Ingot	Lunex Co.
Ruthenium Osmium	99.9+ 99.9+	Powder Powder	Goldsmith Bros., Div. of National Lead
Rhenium	99 . 9 9	Powder	Rembar Co.
Thulium Europium Terbium Ytterbium	99 + 99 + 99 + 99 +	Solid Solid Solid Solid	Michigan Chemical Corp.
Lutetium	99 +	Solid	United Mineral and Chemical Corp.
Cobalt	Spectrographically pure	Sponge	Jarrel Ash Co.
Iron	99.9	Solid	Crane Co. (Metals Div.)
Nickel	99.9+	Solid	International Nickel Co.
Manganese Chromium	99.9+ 99.8	Solid Solid	Union Carbide Metals Co
Molybdenum Tungs t en	99.9+ 99.99	Powder Powder	A. D. Mackay Co.

TABLE II

BINARY RARE EARTH-TRANSITION METAL ALLOYS

IDENTIFIED AS LAVES PHASES

		T -44: 1	D	Α	
	Experimental	This Study	Parameters Other Tr	, A vestigators	-
Alloy	Technique*	a c	a	C	Ref.
	Com	positions of fcc Mg	Cu ₂ Type		
EuIr ₂	LPS	7.566	<u> </u>		
$EuPt_2$	LPS	7.731			
$TbIr_2$	ARC	7. 532			
TbPt ₂	ARC	7.618			
DyIr ₂	ARC	7.517			
DyPt ₂	ARC	7,602	7.5966		(7)
HoPt ₂	ARC	7.591			
ErPt ₂	ARC	7.570			
YbCo ₂	LPS	7.115			
YbRh ₂	LPS	7.432			
YbIr ₂	LPS	7. 477			
LuFe ₂	ARC	7. 217	7. 222		(8)
LuCo ₂	ARC	7.082			
LuNi ₂	ARC	7.064	7.085		(8)
LuRh ₂	ARC	7.422	7.412		(8)
LuIr ₂	ARC	7.462			
	Compos	itions of Hexagonal	Mg Zn ₂ Typ	<u>oe</u>	
$PrOs_2$	LPS	5.370 8.960	5.368±2		(9)
$NdMn_2$	ARC	5.545 9.037			
NdRe ₂	LPS	5.364 8.772			
SmRe ₂	LPS	5.303 8.804			

TABLE II (Continued)

		L	attice Pa	arameters	, A	
	Experimental	This S	-		vestigators	Ref.
Alloy	Technique*	a 5 03/	C 7.43	a		1001,
EuRe ₂	LPS	5, 316	8.742			
$GdRe_2$	LPS	5. 455	8.841			
SmMn ₂	ARC	5.511	8. 976			
TbRu ₂	LPS	5. 254	8.831			
TbRe ₂	LPS	5, 272	8.648			
TbOs ₂	ARC	5.319	8.826			
DyRu ₂	ARC	5, 265	8,852	5. 255	8.844	(10)
DyRe ₂	ARC	5, 391	8.804			
DyOs ₂	ARC	5. 307	8.792			
HoRu ₂	ARC	5, 263	8.827	5.244	8.8099	(10)
HoRe ₂	ARC	5, 378	8.753			
HoOs 2	ARC	5. 295	8.772			
ErRe ₂	ARC	5. 381	8.788			
ErOs ₂	ARC	5. 291	8.755			
TmRu ₂	LPS	5. 246	8.790			
TmRe ₂	LPS	5, 359	8.761			
TmOs ₂	LPS	5. 424	8.808			
YbRu2	LPS	5, 220	8.750			
YbRe2	LPS	5.340	8.685			
YbOs ₂	LPS	5. 244	8.626			
LuMn ₂	ARC	5, 203	8.517	5. 228	8. 590	(10)
LuRe ₂	ARC	5, 317	8.723	5.335	8.717	(10)

^{*} ARC - arc-melted, LPS - liquid-phase sintered.

TABLE III

BINARY RARE EARTH-TRANSITION METAL ALLOYS
IDENTIFIED AS NEITHER MgCu₂ NOR MgZn₂ STRUCTURE

Alloy	Experimental Technique*	Remarks
	No Inte	rmetallic Compounds Found
LaRe ₂	LPS	La + Re + 5 unidentified lines
CeRe ₂	LPS	Ce + Re
$PrRe_2$	LPS	Pr + Re
DyW ₂	ARC	Dy + Wsamples appeared sintered rather than completely melted.
ErMo ₂	ARC	Er + Mo
LuMo ₂	ARC	Lu + Mo
	Other Inte	ermetallic Compounds Present
TbPd ₂	ARC]
DyPd ₂	ADC	
2	ARC	
_	ARC	Same structure(s),
HoPd ₂ ErPd ₂		Same structure(s), not identified.
HoPd ₂	ARC	1

^{*} ARC - arc melted, LPS - liquid-phase sintered.

TABLE IV

TERNARY RARE EARTH-TRANSITION METAL

ALLOYS INVESTIGATED

Alloy	Experi- mental Technique	MgCu ₂	Parame MgZn a	eters, A	Other Phases
		+ Sm)Mn ₂	System		
SmMn ₂			5.511	8.976	
(0.2Er + 0.8Sm)Mn ₂	ARC	7.698			
$(0.4Er + 0.6Sm)Mn_2$	ARC	7.633			
$(0.6Er + 0.4Sm)Mn_2$	ARC	7.611			
$(0.8Er + 0.2Sm)Mn_2$	ARC		5.329	8.704	
ErMn ₂ †			5. 281	8,621	
	(Er	+ Gd)Mn ₂ 5	System		
GdMn2 [†]		7.732			
$(0.2Er + 0.8Gd)Mn_2$	ARC	7.710			
$(0.4Er + 0.6Gd)Mn_2$	ARC	7.633			
$(0.6Er + 0.4Gd)Mn_2$	ARC	7.586	•		
$(0.7Er + 0.3Gd)Mn_2$	ARC	7.569			
$(0.8Er + 0.2Gd)Mn_2$	ARC		5. 327	8.701	
ErMn ₂ [†]			5. 281	8.621	
	<u>(</u> Dy	+ Er)Mn ₂	System		
DyMn ₂ [†]		7.573			
$(0.8Dy + 0.2Er)Mn_2$	ARC	7.569			
$(0.6Dy + 0.4Er)Mn_2$	ARC	7.549			
$(0.5Dy + 0.5Er)Mn_2$	ARC		5.312	8.656	
$(0.4Dy + 0.6Er)Mn_2$	ARC		5.310	8.687	
$(0.2Dy + 0.8Er)Mn_2$	ARC		5. 243	8.616	
ErMn ₂ [†]			5. 281	8.621	

TABLE IV (continued)

	Experi-	Lattic	e Param	eters, A	
	mental	MgCu ₂	MgZn	Type	Other
Alloy 	Technique*	Type, a _o	a _o	c o	Phases
	(Er	+ Ho)Mn ₂	System		
HoMn ₂ [†]		7.507 ±0.005			
(0.9Ho + 0.1Er)Mn ₂	ARC		5, 324	8, 698	
$(0.8 \text{Ho} + 0.2 \text{Er}) \text{Mn}_2$	ARC		5.318	8.684	
$(0.6\text{Ho} + 0.4\text{Er})\text{Mn}_2$	ARC		5.332	8.644	
$(0.4\text{Ho} + 0.6\text{Er})\text{Mn}_2$	ARC		5.302	8.655	
$(0.2\text{Ho} + 0.8\text{Er})\text{Mn}_2$	ARC		5. 298	8.651	
ErMn ₂ [†]			5. 281	8, 621	
	(Dy	+ Tm)Mn ₂ -	System		
DyMn ₂ [†]		7.5731			
$(0.8Dy + 0.2Tm)Mn_2$	ARC	7.561			
$(0.6Dy + 0.4Tm)Mn_3$	ARC		5.325	8.685	
(0.4Dy + 0.6Tm)Mn ₂	ARC		5. 298	8.676	
$(0.2Dy + 0.8Tm)Mn_2^2$	ARC		5, 293	8.630	
TmMn ₂ [†]			5. 241	8, 565	
	(Ho	+ Tm)Mn2	System		
HoMn ₂ [†]		7, 507 ±0, 005			
(0.9Ho + 0.1Tm)Mn ₂	ARC	7.522			
$(0.8\text{Ho} + 0.2\text{Tm})\text{Mn}_2^2$	ARC		5, 311	8.695	
(0.6Ho + 0.4Tm)Mn ₂	ARC		5. 292	8.615	
$(0.4 \text{Ho} + 0.6 \text{Tm}) \text{Mn}_2$	ARC		5. 272	8.590	
(0.2Ho + 0.8Tm)Mn ₂	ARC		5. 282	8,623	
TmMn ₂ [†]			5, 241	8. 565	

TABLE IV (continued)

	Experi-		Param	eters, A	<u>4</u>	
Alloy	mental- * Technique	MgCu ₂ Type, a _o	$\frac{\text{Mg Zn}}{a}$	Type c		Other Phases
	Er(Cr	+ Mn) ₂ Sys	stem			
ErCr ₂ [†]					E	Er + Cr ,
$Er(0.8Cr + 0.2Mn)_2$	ARC				E	Er + Cr
$Er(0.6Cr + 0.4Mn)_2$	ARC	5	. 261	8.598	E	Er + Cr
$Er(0.4Cr + 0.6Mn)_2$	ARC	5	. 266	8.631		
$Er(0.2Cr + 0.8Mn)_2$	ARC	5	. 166	8.436		
ErMn ₂		5	. 281	8,621		
	Tm(C	$r + Mn)_2 Sy$	rstem			
TmCr ₂					7	[m + Cr (
$Tm(0.8Cr + 0.2Mn)_2$	ARC	5	. 295	8.585	7	[m + Cr
$Tm(0.6Cr + 0.4Mn)_2$	ARC	5	.300	8.675	7	[m
$Tm(0.4Cr + 0.6Mn)_2$	ARC	5	. 262	8.590	7	r m
$Tm(0.2Cr + 0.8Mn)_2$	ARC	5	. 232	8.520		
TmMn2 [†]		5	. 241	8.565		
	Lu(C	r + Mn) ₂ Sy	stem			
LuCr ₂					I	Lu + Cr (
$Lu(0.8Cr + 0.2Mn)_2$	ARC	5	. 220	8.530	J	Lu + Cr
$Lu(0.6Cr + 0.4Mn)_2$	ARC	5	. 103	9.066	J	Lu + Mn
$Lu(0.4Cr + 0.6Mn)_2$	ARC	5	. 219	8.511]	Lu + Mn
$Lu(0.2Cr + 0.8Mn)_2$	ARC	5	. 235	8.535]	Lu + Mn
LuMn ₂	ARC	5	. 203	8.517		

TABLE IV (continued)

Alloy $\frac{\text{mental}}{\text{Technique}}^*$ $\frac{\text{MgCl}_2}{\text{Type, a}_0} \frac{\text{MgZn}_2}{\text{a}_0} \frac{\text{Type}}{\text{c}_0}$ Other Phases $\frac{\text{Er}(\text{Mn} + \text{Fe})_2 \text{ System}}{\text{System}}$ Er\(\text{Mn}_2^\frac{\dagger{\partial}{\part		Experi-	Lattic	e Paran	eters,	A	
Alloy Technique Type, a_0 a_0 c_0 Phases $ \frac{\text{Er}(\text{Mn} + \text{Fe})_2 \text{ System}}{5.281} = 8.621 $ $ \text{Er}(0.8 \text{Mn} + 0.2 \text{Fe})_2 = 5.255 = 8.596 $ $ \text{Er}(0.7 \text{Mn} + 0.3 \text{Fe})_2 = 7.425 $ $ \text{Er}(0.6 \text{Mn} + 0.4 \text{Fe})_2 = 7.398 $ $ \text{Er}(0.4 \text{Mn} + 0.6 \text{Fe})_2 = 7.353 $ $ \text{Er}(0.2 \text{Mn} + 0.8 \text{Fe})_2 = 7.314 $ $ \text{Er}\text{Fe}_2^{\dagger} = 7.274 $ $ \frac{\text{Tm}(\text{Mn} + \text{Fe})_2 \text{ System}}{5.241} = 8.565 $ $ \text{Im}(0.8 \text{Mn} + 0.2 \text{Fe})_2 = 7.348 = 5.172 = 8.466 $ $ \text{Im}(0.6 \text{Mn} + 0.4 \text{Fe})_2 = 7.289 $ $ \text{Im}(0.2 \text{Mn} + 0.8 \text{Fe})_2 = 7.279 $ $ \text{Im}(0.2 \text{Mn} + 0.8 \text{Fe})_2 = 7.247 $ $ \frac{(\text{La} + \text{Nd})\text{Os}_2}{7.247} $ $ \frac{(\text{La} + \text{Nd})\text{Os}_2}{7.736} $ $0.8 \text{La} + 0.2 \text{Nd})\text{Os}_2 = 5.375 = 8.983 $ $0.6 \text{La} + 0.4 \text{Nd})\text{Os}_2 = 5.375 = 8.983 $ $0.4 \text{La} + 0.6 \text{Nd})\text{Os}_2 = 5.366 = 8.966 $ $0.2 \text{La} + 0.8 \text{Nd})\text{Os}_2 = 5.368 = 8.926 $		mental *	$^{ m MgCu}_2$	MgZn	Type		Other
$\frac{\text{Er}(\text{Mn} + \text{Fe})_2 \text{System}}{\text{5.281}} = 8.621$ $\text{Er}(0.8 \text{Mn} + 0.2 \text{Fe})_2 = 5.255 = 8.596$ $\text{Er}(0.7 \text{Mn} + 0.3 \text{Fe})_2 = 7.425$ $\text{Er}(0.6 \text{Mn} + 0.4 \text{Fe})_2 = 7.398$ $\text{Er}(0.4 \text{Mn} + 0.6 \text{Fe})_2 = 7.353$ $\text{Er}(0.2 \text{Mn} + 0.8 \text{Fe})_2 = 7.314$ $\text{Er}(0.2 \text{Mn} + 0.8 \text{Fe})_2 = 7.274$ $\frac{\text{Tm}(\text{Mn} + \text{Fe})_2 \text{System}}{5.241} = 8.565$ $\text{Im}(0.8 \text{Mn} + 0.2 \text{Fe})_2 = 7.348 = 5.172 = 8.466$ $\text{Im}(0.4 \text{Mn} + 0.6 \text{Fe})_2 = 7.289$ $\text{Im}(0.4 \text{Mn} + 0.6 \text{Fe})_2 = 7.247$ $\text{Im}(0.2 \text{Mn} + 0.8 \text{Im}(0.2 \text{Mn})_2 = 7.247$ $\text{Im}(0.2 \text{Mn} + 0.8 \text{Im}(0.2 \text{Mn})_2 = 7.247$ $\text{Im}(0.2 \text{Mn} + 0.8 \text{Im}(0.2 $	Alloy	Technique	Type, a o	a _o	c _o		Phases
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		Er(N	In + Fe)2	System		-	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	ErMn ₂ [†]				8.621		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$Er(0.8Mn + 0.2Fe)_2$			5. 255	8. 596		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$Er(0.7Mn + 0.3Fe)_2$		7.425				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$Er(0.6Mn + 0.4Fe)_2$		7.398				
$\frac{\text{Tm}(\text{Mn} + \text{Fe})_2}{\text{Tm}(\text{Mn} + \text{Fe})_2} \frac{\text{System}}{\text{5. 241}} = \frac{\text{Tm}(\text{Mn} + \text{Fe})_2}{\text{5. 226}} = \frac{\text{System}}{\text{5. 172}} = \frac{\text{System}}{\text{5. 241}} = \frac{\text{System}}{\text{5. 226}} = \frac{\text{System}}{\text{5. 249}} = \frac{\text{System}}{\text{5. 375}} = \text{S$	$Er(0.4Mn + 0.6Fe)_2$		7.353				
$\frac{\text{Tm}(\text{Mn} + \text{Fe})_2}{\text{System}} = \frac{\text{System}}{5.241} = \frac{8.565}{8.573}$ $\frac{\text{Tm}(0.8 \text{Mn} + 0.2 \text{Fe})_2}{5.226} = \frac{8.573}{8.466}$ $\frac{\text{Tm}(0.6 \text{Mn} + 0.4 \text{Fe})_2}{7.289} = \frac{7.289}{7.247}$ $\frac{\text{Tm}(0.2 \text{Mn} + 0.8 \text{Fe})_2}{7.247} = \frac{7.247}{7.247}$ $\frac{(\text{La} + \text{Nd})\text{Os}_2}{7.736} = \frac{\text{System}}{7.736}$ $\frac{(\text{La} + \text{Nd})\text{Os}_2}{7.740} = \frac{8.913}{5.375} = \frac{9.93}{8.983}$ $\frac{0.6 \text{La} + 0.4 \text{Nd})\text{Os}_2}{0.4 \text{La} + 0.6 \text{Nd})\text{Os}_2} = \frac{5.366}{5.368} = \frac{9.66}{8.966}$ $\frac{1.368}{1.368} = \frac{9.26}{1.368}$	$Er(0.2Mn + 0.8Fe)_2$		7.314				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ErFe ₂ [†]		7.274				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							
Tm(0.8Mn + 0.2Fe) ₂ Tm(0.6Mn + 0.4Fe) ₂ Tm(0.4Mn + 0.6Fe) ₂ Tm(0.2Mn + 0.8Fe) ₂ TmFe ₂ TmFe ₂ (La + Nd)Os ₂ T.736 0.8La + 0.2Nd)Os ₂ 0.6La + 0.4Nd)Os ₂ 0.4La + 0.6Nd)Os ₂ 0.2La + 0.8Nd)Os ₂ NdOs ₂ Tm(0.8Mn + 0.2Fe) ₂ T.348 5.172 8.466 T.289 T.279 T.247 (La + Nd)Os ₂ T.736 T.740 5.391 8.913 5.375 8.983 5.429 8.889 5.366 8.966 5.368 8.966 5.368 8.926	4	Tm($\frac{Mn + Fe}{2}$	System			
Tm(0.6Mn + 0.4Fe) ₂ Tm(0.4Mn + 0.6Fe) ₂ Tm(0.2Mn + 0.8Fe) ₂ TmFe ₂	TmMn ₂ ¹			5. 241	8.565		
$Tm(0.4Mn + 0.6Fe)_2$ $Tm(0.2Mn + 0.8Fe)_2$ $TmFe_2^{\dagger}$ 7.289 7.279 7.247 $\frac{(La + Nd)Os_2}{7.736} \frac{System}{7.736}$ $0.8La + 0.2Nd)Os_2$ $0.6La + 0.4Nd)Os_2$ $0.4La + 0.6Nd)Os_2$ $0.2La + 0.8Nd)Os_2$ $0.2La + 0.8Nd)Os_2$ $0.3La + 0.8Nd)Os_2$ $0.3La + 0.3Nd)Os_2$	Tm(0.8Mn + 0.2Fe) ₂			5. 226	8.573		
$Tm(0. 2Mn + 0. 8Fe)_2$ $TmFe_2^{\dagger}$ $7. 279$ $7. 247$ $\frac{(La + Nd)Os_2}{7. 736} \frac{System}{7. 736}$ $0. 8La + 0. 2Nd)Os_2$ $0. 6La + 0. 4Nd)Os_2$ $0. 4La + 0. 6Nd)Os_2$ $0. 2La + 0. 8Nd)Os_2$ $0. 2La + 0. 8Nd)Os_2$ $0. 366$ 0	$Tm(0.6Mn + 0.4Fe)_2$		7.348	5.172	8. 466		
7. 247 (La + Nd)Os ₂ System 7. 736 0. 8La + 0. 2Nd)Os ₂ 0. 6La + 0. 4Nd)Os ₂ 0. 4La + 0. 6Nd)Os ₂ 0. 2La + 0. 8Nd)Os ₂ NdOs ₂ 7. 740 5. 391 8. 913 5. 375 8. 983 5. 429 8. 889 5. 366 8. 966 5. 368 8. 926	Tm(0.4Mn + 0.6Fe) ₂		7.289				
(La + Nd)Os ₂ System 7.736 0.8La + 0.2Nd)Os ₂ 7.740 5.391 8.913 0.6La + 0.4Nd)Os ₂ 5.375 8.983 0.4La + 0.6Nd)Os ₂ 0.2La + 0.8Nd)Os ₂ NdOs ₂ 5.366 8.966 5.368 8.926	$Tm(0.2Mn + 0.8Fe)_2$		7.279				
7.736 0.8La + 0.2Nd)Os ₂ 0.6La + 0.4Nd)Os ₂ 0.4La + 0.6Nd)Os ₂ 0.2La + 0.8Nd)Os ₂ NdOs ₂ 7.736 7.740 5.391 8.913 5.429 8.889 5.429 8.889 5.366 8.966 8.966	TmFe ₂		7. 247				
7.736 0.8La + 0.2Nd)Os ₂ 0.6La + 0.4Nd)Os ₂ 0.4La + 0.6Nd)Os ₂ 0.2La + 0.8Nd)Os ₂ NdOs ₂ 7.736 7.740 5.391 8.913 5.429 8.889 5.429 8.889 5.366 8.966 8.966							
0.8La + 0.2Nd)Os ₂ 7.740 5.391 8.913 0.6La + 0.4Nd)Os ₂ 5.375 8.983 0.4La + 0.6Nd)Os ₂ 5.429 8.889 0.2La + 0.8Nd)Os ₂ 5.366 8.966 NdOs ₂ 5.368 8.926	†	(<u>La</u> +		ystem			
0.6La + 0.4Nd)Os ₂ 5.375 8.983 0.4La + 0.6Nd)Os ₂ 5.429 8.889 0.2La + 0.8Nd)Os ₂ 5.366 8.966 NdOs ₂ 5.368 8.926	4						
0. 4La + 0. 6Nd)Os ₂ 0. 2La + 0. 8Nd)Os ₂ 5. 429 8. 889 5. 366 8. 966 5. 368 8. 926	4		7.740				
0. 2La + 0.8Nd)Os ₂ 5. 366 8. 966 NdOs ₂ 5. 368 8. 926	4						
NdOs ₂ [†] 5.368 8.926	4						
	NaOs 2			5.368 ±.002	8.926 ±.001		

TABLE IV (continued)

		Lattic	e Param	eters, A	
	Experi-	MgCu ₂	Mg Zn ₂	Type	Other
Alloy	mental * Technique	Type, a	a _o	co	Phases
	(La -	Gd)Os 2 S	ystem		
LaOs ₂ [†]		7.737 ±0.001			
(0.8La + 0.2Gd)Os ₂	LPS	7.741	5.328	8.694	
$(0.6La + 0.4Gd)Os_2$	LPS		5.373	8.948	
$(0.4La + 0.6Gd)Os_2$	LPS		5. 327	8.838	
$(0.2La + 0.8Gd)Os_2$	LPS		5, 336	8.860	
GdOs ₂ [†]			5.319 ±0.002	8.838 ±0.002	
	(Ce ·	+ Gd)Os ₂ S	ystem		
CeOs ₂ [†]		7.593 ±0.001			
(0.8Ce + 0.2Gd)Os ₂	LPS		5.330	8.847	
(0.6Ce + 0.4Gd)Os ₂	LPS		5.333	8.825	
$(0.4Ce + 0.6Gd)Os_2$	LPS		5.324	8, 837	
$(0.2Ce + 0.8Gd)Os_2$	LPS		5.335	8,860	
GdOs ₂ [†]			5.319 ±0.002	8.838 ±0.002	
	(Sm	+ Gd)Ru ₂ S	System		
SmRu ₂ [†]	<u></u>	7. 580			
(0.8Sm + 0.2Gd)Ru ₂	LPS	7.577	5. 292	8.865	
(0.6Sm + 0.4Gd)Ru ₂			5.280	8. 922	
(0.4Sm + 0.6Gd)Ru ₂			5. 283	8.914	
(0. 2Sm + 0. 8Gd)Ru ₂	•		5. 298	8. 927	
GdRu ₂ [†]	•		5. 271	8.904	
4			±0.002	±0.002	

^{*} ARC - arc melted, LPS - liquid-phase sintered.

[†] Parameter values taken from literature.

A — ELEMENT			B – EL	B - ELEMENT		
	>	Cr	Z Z	F e	°	Ë
Zr		*				
q O						
Ŧ		*				
		MgCu ₂	N	MgZn ₂		

Fig. 1 - CRYSTAL STRUCTURES OF TRANSITION METAL-TRANSITION METAL LAVES PHASES.

DEPENDENT ALLOTROPY

*TEMPERATURE

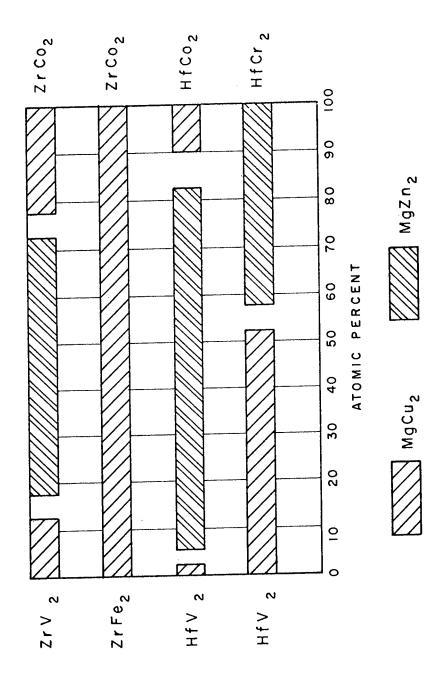


Fig. 2 - TERNARY MISCIBILITY BETWEEN TRANSITION METAL-TRANSITION METAL LAVES PHASES.

B - ELEMENT I∇a Хa $\nabla \mathbf{I}$ a MIO MIO MIP MIC Ti V CrFe Co Mn Ni NC. Х NC Sc 1.12* 1.21 1.28 1.20 1.27 1.30 1.31 NC N C NC Υ 1.22 1.32 1.41 1.31 1.40 1.43 1.44 NC NC NC NC NC Х La 1.50 1.28 1.38 1.47 1.37 1.46 1.49 NC NC NC N C Сe 1.24 1.35 1.43 1.34 1.45 1.42 1.46 Х NC Х X X Pr 1.24 1.35 1.43 1.34 1.42 1.45 1.46 N C N C Х Nd 1.24 1.34 1.42 1.33 1.41 1.44 1946 Χ Χ Х Х X Х Pm 1.23 1.33 1.41 1.39 1.42 1.44 1.44 Χ Х Х Sm 1.22 1.41 1.32 1.31 1.43 1.40 1.44 Χ Χ Χ Х Eu A - ELEMENT 1.39 1.50 1.59 1.49 1.58 1.62 1.63 NC NC NC Gd 1.22 1.32 1.41 1.31 1.40 1.43 1.44 Х Х Χ Х Tb 1.21 1.31 1.39 1.30 1.38 1.41 1.42 NC NC NC Dy 1.20 1.30 1.38 1.29 1.37 1.40 1.42 NC Х Х Нο 1.20 1.40 1.30 1.38 1.29 1.37 1.42 NC Х NC Er 1.20 1.29 1.38 1.28 1.36 1.40 1.41 X Х X X Tm 1.19 1.29 1.37 1.28 1.36 1.39 1.40 Х X Х Х Х Υb 1.32 1.43 1.52 1.42 1.50 1.54 1.55 X NC X Lu 1.18 1.27 1.35 1.26 1.34 1.37 MgZn₂ MgCu₂ KEY:

Fig. 3 - CRYSTAL STRUCTURES OF LAVES PHASES FORMED BETWEEN THE RARE EARTH ELEMENTS AND METALS OF THE FIRST TRANSITION SERIES.

NC , NO COMPOUND

X, UNKNOWN

B - ELEMENT

		ΙV.a	Vσ	ΣΙα	XII a	VIII a	VIII b	УШ с
		Zr	Cb	Мо	(Tc)	Ru	Rh	Pd
A-ELEMENT	s c	х	x	х			X	Х
		1.01*	1,12	1.17		1.24	1.21	1, 19
	Y	N C	NC	NC				X
		1.11	1.22	1.29		1.36	1.33	1.30
	1					K	~~~	
	La	NC	NC	NC		7777		X 1.36
		1,16	1.28	1.34		1.42	1.39	1.36 X
	Се	NC	NC	NC		7777	1.36	1.33
		1.13	1.24	1.31		1.39	7.77	
	Pr	X	Х	X		777	7777	×
		1.13	1.24	1.31		1.39	1.36	1.33
	Nd.	Х	X	X		7777	777,	X
		1.12	1.24	1.30		1.38	1.35	1.32
	Ρm	X 1.13	X 1.23	X 1.29		1.35	1,35	1.32
	Sm	X	X	Х	1	7777	×	X
		1.11	1.22	1.29		1.36	1.33	1.30
	Εu	Х	X	×		X	X	X
		1.26	1.39	1.46		1.55	1.51	1.48
	Gd	NC	NC	N.C	1		777,	X
		1.11	1.22	1.29		1.36	1.33	1.30
	Тb	×	X	×	}		1 ×	X
		1.10	1.21	1.34	ļ	1.35	1.32	1.29 X
	D y	NC	NC	NC			1:31	1.28
		1.09	1.20	1.26	ļ	1.34	1.31	
	Но	×	×	_ X	1		<u> </u>	X 1.28
		1.09	1.20	1.26	<u> </u>	1.34	1.31	1.28 X
	Er	NC	X	NC	ļ	1.34	1.30	1.28
		1.09	1.20	1.25	<u> </u>	1.34		x x
	Tm	X	X	X		1 3 3	X 1.30	1.27
		1.08	1.19	1.25	 	1.33	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	X X
	Y b L·u	X	X	X	1	1.47	1.44	1.41
		1.20	1.32	1.39		177	/ 	X
		X	X	NC 1.24		1.31	1.28	1.25
		I.07 KEY:	1.18		MgZn	2	777	Mg Cu ₂
	* dA X, UNKNOWN NC, NO COMPO							

Fig. 4 - CRYSTAL STRUCTURES OF LAVES PHASES FORMED BETWEEN THE RARE EARTH ELEMENTS AND METALS OF THE SECOND TRANSITION SERIES.

X, UNKNOWN NC, NO COMPOUND dB

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Fig. 5 - CRYSTAL STRUCTURES OF LAVES PHASES FORMED BETWEEN THE RARE EARTH ELEMENTS AND METALS OF THE THIRD TRANSITION SERIES.

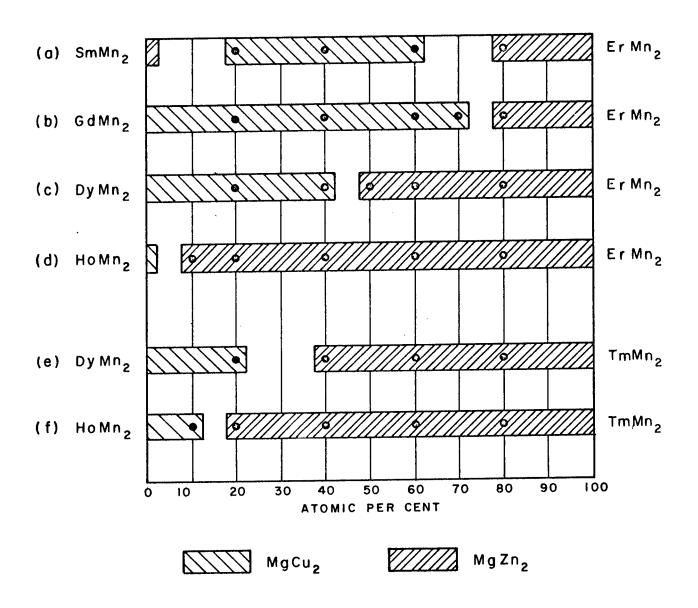


Fig. 6 - TERNARY MISCIBILITY OF RARE EARTH ELEMENT-TRANSITION METAL LAVES PHASES, I.

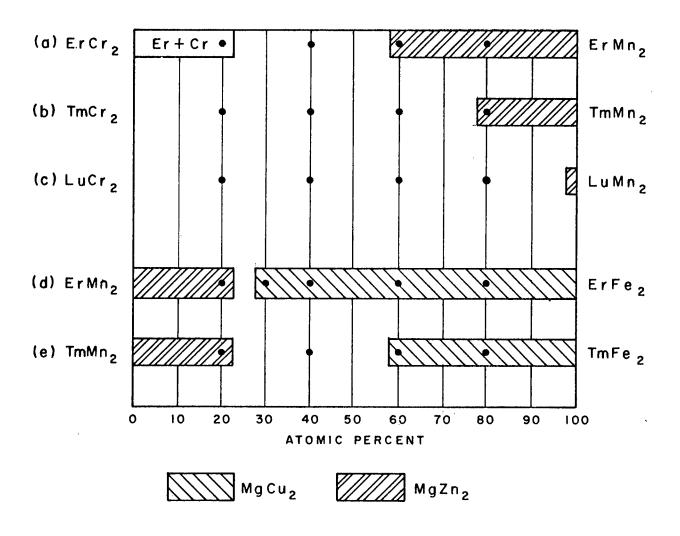


Fig. 7 - TERNARY MISCIBILITY OF RARE EARTH ELEMENT-TRANSITION METAL LAVES PHASES, II.

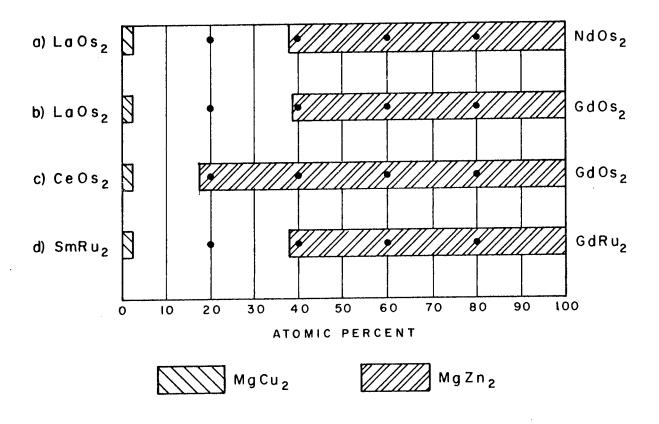


Fig. 8 - TERNARY MISCIBILITY OF RARE EARTH ELEMENT-TRANSITION METAL LAVES PHASES, III.

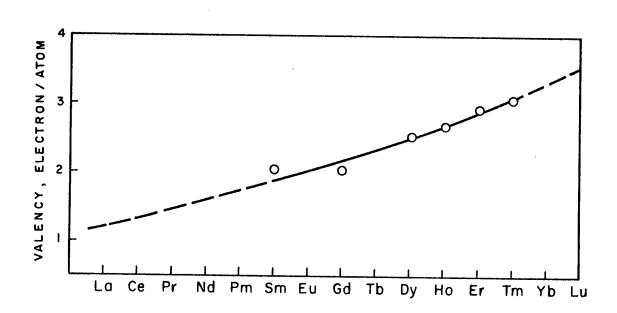


Fig. 9 - VALENCIES OF THE RARE EARTH ELEMENTS.